

# Interdependency Analysis in Electric Power Systems

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# Outline

- ❖ **Context and objectives**
- ❖ **The analyzed Electrical Power System instance**
  - ✓ **The electrical infrastructure**
  - ✓ **The Information technology based control system**
- ❖ **The Interdependencies between EI and ITCS**
- ❖ **The SAN model of the EPS instance**
- ❖ **The analyzed case study and measure of interest**
- ❖ **The results of the analyses**
- ❖ **Final considerations and future developments**

# The context

- Economy, security and quality of life increasingly depend on the resiliency of a number of **critical infrastructures**
- **Interdependencies** increase vulnerability of CI, as they give rise to multiple error propagation channels from one infrastructure to another

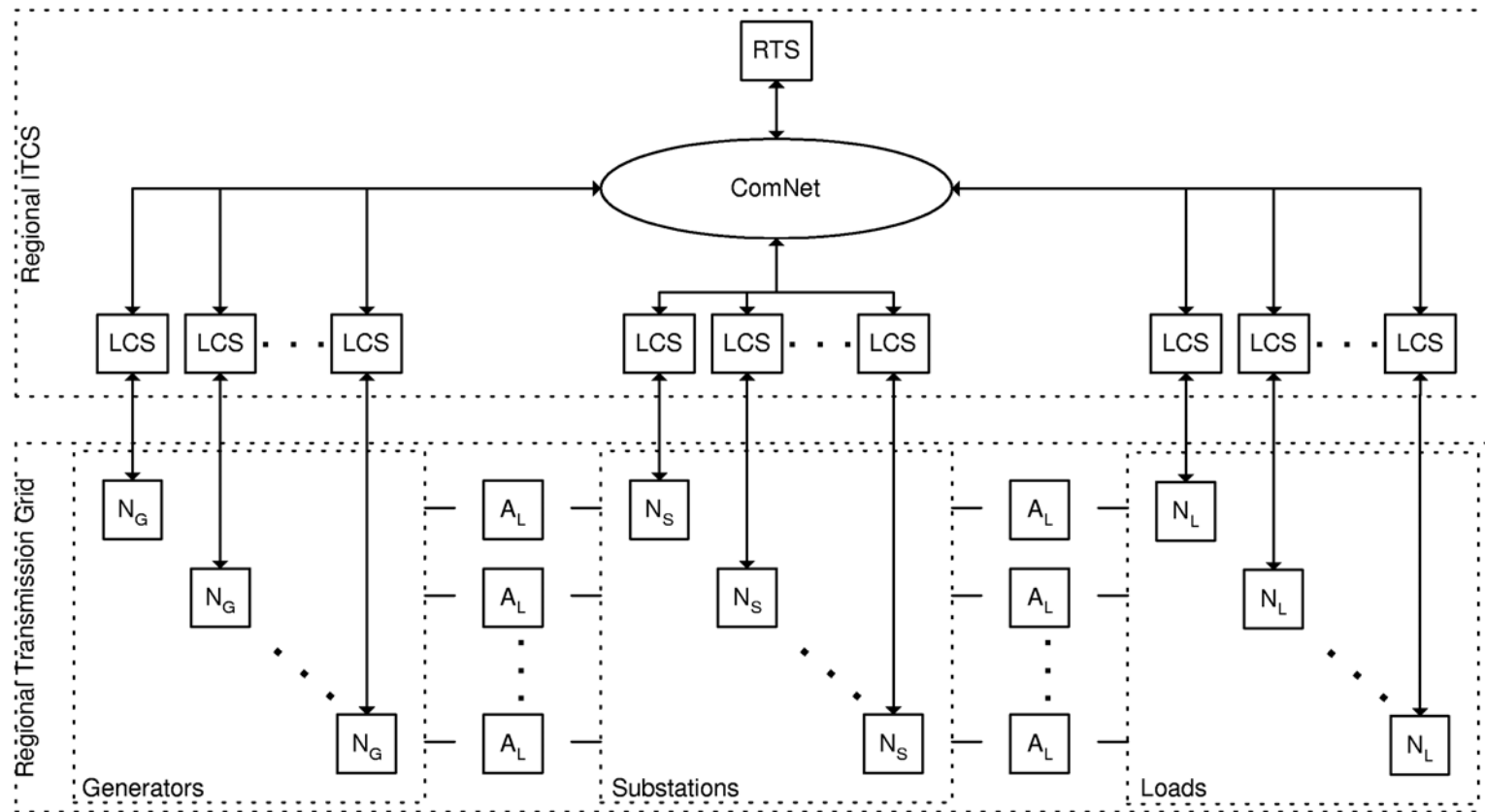
**→ Analysis of infrastructures components interactions is crucial to understand and characterize interdependencies**

- **Electrical Power Systems** are prominent representatives of CI
- Interdependencies between the electrical power grid (**EI**) and the control system infrastructure (**ITCS**) have been responsible of major power grid blackouts
- The EU STREP 027513 **CRUTIAL** project is addressing the analysis and management of interdependencies and of the resulting operational risk

# Objective

- Define a conceptual **modeling framework** well suited to characterize and analyze the **interdependencies** between
  - the information infrastructure
  - the controlled power infrastructure
- With focus on **interdependence-related failures**
- Aiming at **quantitatively assessing** their impact on the resilience of EPS
- Adopting a compositional approach, where building-blocks represent basic components/events, and through their composition potentially any EPS configurations can be represented
  
- **In this paper**
  - **application of the developed modeling framework to a case study**
  - **to assess a blackout-related indicator**
  - **under different system conditions**

# Logical structure of the analyzed EPS instance



# Interdependencies

- $\mathbf{S}_{ITCS} \rightarrow \mathbf{S}_{EI}$ 
  - Impact on topology and/or the electric values
    - ✓ E.g. a value failure of LCS (incorrect closing or opening of the power line  $A_L$ )
- $\mathbf{S}_{EI} \rightarrow \mathbf{S}_{ITCS}$ 
  - E.g. A failure in the EI causes a partial black-out that could reduce the performance of the private or public networks used by ITCS, or isolate part of the ITCS.
- $(\mathbf{S}_{EI} \text{ and } \mathbf{S}_{ITCS}) \rightarrow (\mathbf{S}_{EI} \text{ or } \mathbf{S}_{ITCS})$ 
  - E.g. An ITCS component fails (omission failure) and does not isolate an EI component affected by a disruption  $\rightarrow$  the grid topology changes (the disruption propagates and a set of contiguous EI components may become disrupted)

# Major implementation assumptions

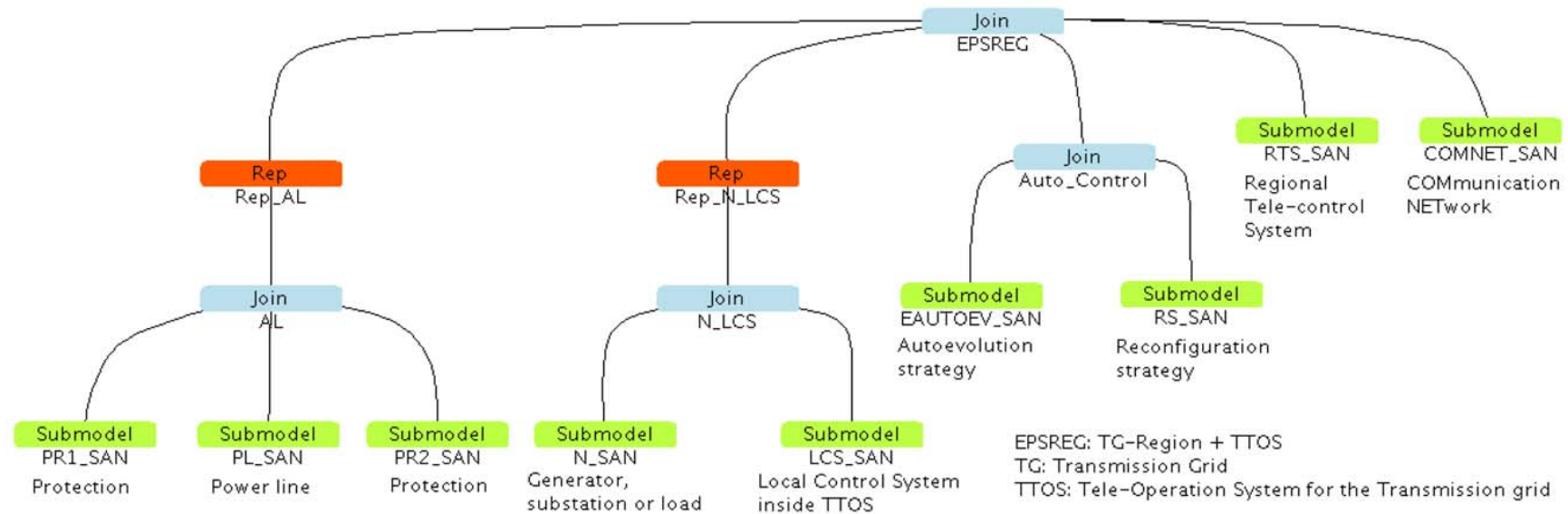
## □ On EI:

- The EI state and evolution is determined by the equations for the DC power flow approximation (derived from the standard AC circuit equations), which give a **linear relationship** to assure equilibrium between:
  - ✓ the **power at the nodes (generators, loads or substation)** and
  - ✓ the **power flow on the lines**

## □ On ITCS:

- **Local operations** performed by LCS are represented by the **reconfiguration function  $RS_1()$** , while
- **Global operations** performed by RTS are represented by the **reconfiguration function  $RS_2()$**
- definition of  **$RS_1()$**  and  **$RS_2()$**  depends on the policies and algorithms adopted by the Regional ITCS. They are obtained by solving a **linear programming problem while minimizing a cost function**
  - ✓ The new state determined by  **$RS_1()$**  is suboptimal wrt  **$RS_2()$**  (being based on local information);
  - ✓  **$RS_1()$**  completes in time  **$T_1=0$** , while  **$RS_2()$**  in time  **$T_2>0$**

# The Composed Model using Möbius and SAN



- **Rep\_AL**: nA non anonymous replicas of the model AL
- **Rep\_N\_LCS**: nN non anonymous replicas of the model N\_LCS
- The submodels interact through **common places**





# Measure of interest

- $P_{UD}(t,t+1)$ : *percentage of the mean power demand that is not met in the interval  $[t,t+1]$  hours*  
(the symbol 'UD' stands for 'Unsatisfied Demand').

It is a user-oriented measure of the **blackout size** and has been obtained as the load shed (i.e., the not served power due to a load shedding) divided by the power demand.

# Analyzed scenario

**GOAL:** to assess the impact of the **omission failure of the communication network** (ComNet) on  $P_{UD}(t,t+1)$  in presence of a **simultaneous failure of a set of transmission lines**.

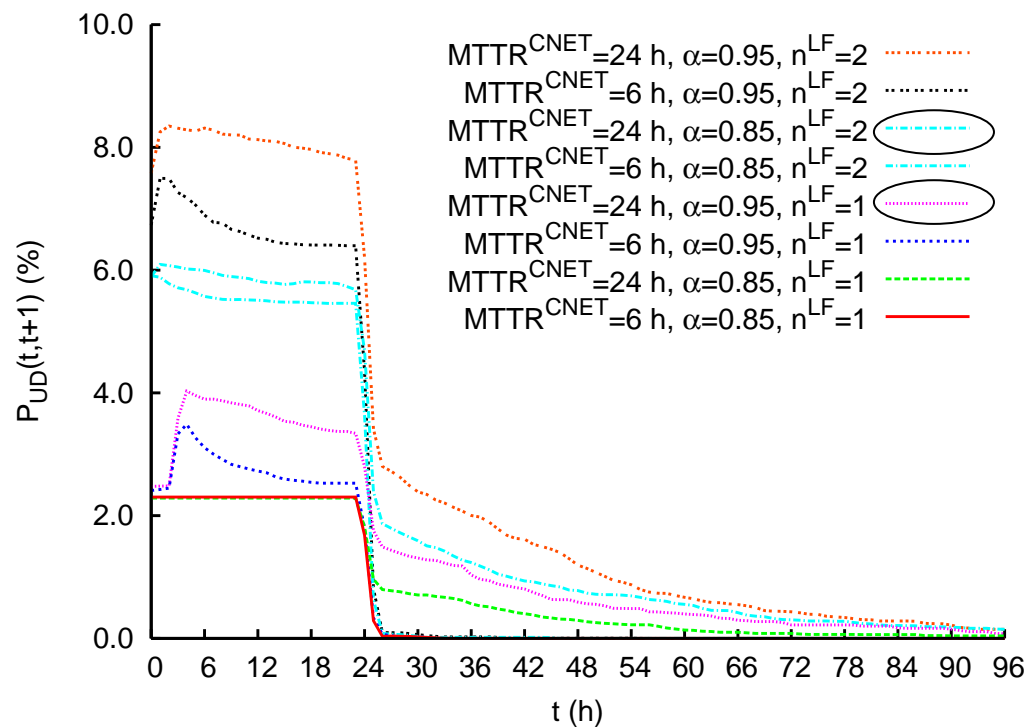
More in detail:

- The grid starts in electrical equilibrium.
- At time zero,  $n^{LF}$  **power lines are simultaneously affected by a permanent failure** (e.g., due to a tree fall or a terrorist attack), thus becoming unavailable.
  - The power lines that fail are randomly (*uniformly*) selected from the set of all available power lines.
  - All the failed power lines are (*deterministically*) repaired after 24 hours.
- At the same time zero, **ComNet is simultaneously affected by a denial of service (DoS) attack**.
  - The DoS attack ends after an *exponentially* distributed time with mean  $MTTR^{CNET}$ , and from that time RTS can start computing the RTS reconfiguration action that will be (*deterministically*) applied after 10 minutes.

# Sensitivity analysis campaign

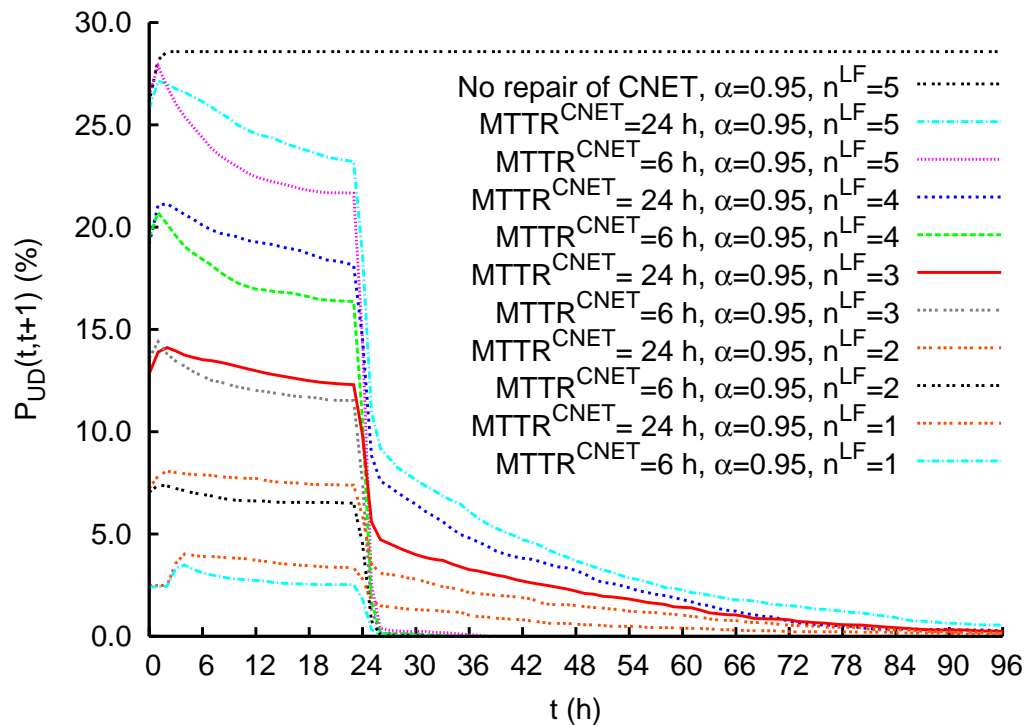
- A sensitivity analysis has been performed on the following parameters:
  - $MTTR^{CNET}$ , thus **varying the duration of the DoS attack** affecting the communication network.  $MTTR^{CNET}$  induces a delay on RTS operation (RTS omission failure).
  - $n^{LF}$ , thus **varying the severity of the overall EI failure**.
  - $\alpha$ , thus **varying the initial stress level of the power grid**.
    - ✓ For each generator  $i$ ,  $\alpha$  is defined as the ratio  $P_i/P_i^{max}$ .
    - ✓ In the initial grid setting all the ratios  $P_i/P_i^{max}$  are equal to a fixed value  $\alpha=0.85$ .

## $P_{UD}(t,t+1)$ , with $t=0,1,\dots,96$ h., for different values of $MTTR^{CNET}$ (6, 24 h.), $n^{LF}$ (1, 2) and $\alpha$ (0.85, 0.95)



- The failure of even a single line produces and immediate increment of  $P_{UD}(t,t+1)$  due to lines overloading and to too big variation of power demand to generators in a small interval of time.
- At  $t=24$  hours there is a big improvement (the failed power lines are repaired).
- The impact of the system stress level  $\alpha$  is less heavy than the failure of power lines

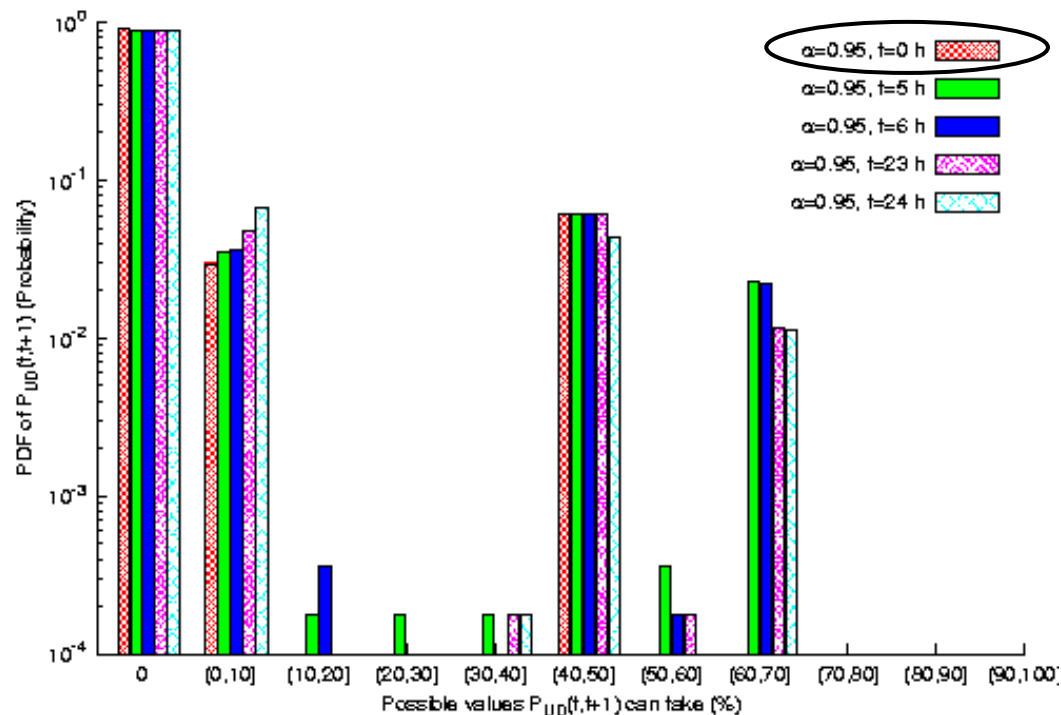
## $P_{UD}(t,t+1)$ , with $t=0,1,\dots,96$ hours, for different values of $MTTR^{CNET}$ (6, 24 h.) and $n^{LF}$ (1,...,5), fixing $\alpha=0.95$



- $P_{UD}(t,t+1)$  increases considering higher  $n^{LF}$  values, and fixing the value for  $n^{LF}$ ,  $P_{UD}(t,t+1)$  gets worse in the case in which the DoS attack has a longer duration (24 hours).
- After 24 hours the disrupted power lines are repaired, and consequently  $P_{UD}(t,t+1)$  rapidly decreases until reaching the zero value.
- The top most curve represents the case of RTS omission failure

# Probability that $P_{UD}(t, t+1)$ is in the intervals $(0, 10]\%$ , $(10, 20]\%$ , ... , $(90, 100]\%$ , fixing $\alpha=0.95$ , $n^{LF}=1$ and $MTTR^{CNET}=24$ hours

From previous figures  $P_{UD}(0,1) \approx 2.5$ .



Analyzing its complete distribution:

- with a very high probability the % of undelivered power is zero;
- $P_{UD}(0,1)$  is in  $(0,10]\%$  with a probability  $\sim 0.03$ , and it is in  $(40,50]\%$  with a probability  $\sim 0.06$ ;
- all the other probabilities are almost zero.

A mean loss of 40-50% of delivered power in the first hour of the system can happen, for example, when the power line affected by the failure is directly connected to a generator.

# Some considerations

- ❑ The obtained results allow to understand some relevant dynamics in failures propagation and their impact through infrastructures interdependencies.
- ❑ ***Such insights can be usefully exploited towards proper system configurations enhancing resiliency and survivability.***
- ❑ E.g., the EPS analysis under **different stress levels** is useful to find a **proper configuration of the power grid so to limit the power lines overloading in case of failures.**
- ❑ Also, understanding the effect of **repair times** of the communication network allows to **better calibrate repair operations to enhance system availability.**



# Conclusions

- ❑ We addressed the modeling of EPS and a quantitative assessment of the impact of failures through interdependencies between the information control infrastructure and the controlled electric grid.
- ❑ We have modeled an instance of EPS made up of a regional tele-operation system and the local control systems connected to it.
- ❑ Simulation analyses have been performed on a portion of the IEEE 118 Bus Test Case, to evaluate the user perceived degradation of the power demand satisfaction under varying failures and system conditions.
- ❑ Usefulness of such analyses towards improving system survivability and availability has been briefly discussed

# Ongoing and future work

- Simulations to identify the most critical power lines for a given topology
- Detailed analysis and description of the EI grid's evolution through observing simulation runs
- Extension of the experimental campaign
  - by including the failures of other EI components
    - ✓ e.g., protections
  - by including other kinds of failures
    - ✓ e.g., lightning affecting power lines
  - by introducing other patterns of components failures
    - ✓ e.g., sequences of clusters of simultaneous failures
    - ✓ e.g., DoS attacks restricted to the portion of ComNet connecting a subset of LCS
  - by enriching the set of measures of interest for the analyses
    - ✓ e.g., time to reach a certain black-out level
    - ✓ e.g., number of failed power lines/nodes in a certain interval of time